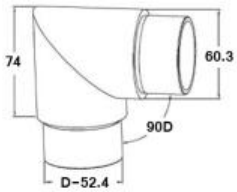
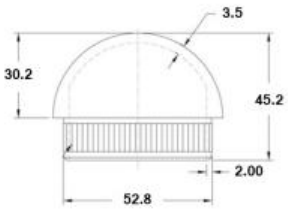
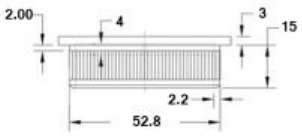


RV1005-60.3-316
90 Degree Sharp Ben

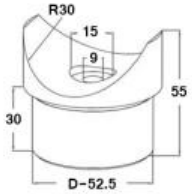
RV1001-60.3-316
Straight Tube Connector



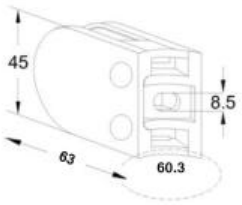
W270-4mm
Dome End Cap



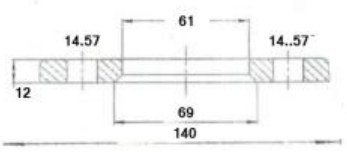
W268-4mm
Flat End Cap



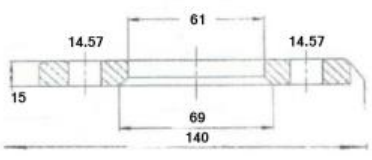
RA1006-60.3-316
Top Rail Insert



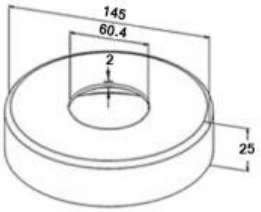
KLH10D-60.3
Glass Clamp 304/316G - Satin
Rubbers also available for 6/8/12mm Glass



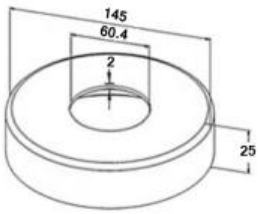
RON140-12
Weldable Base Plate
304/316



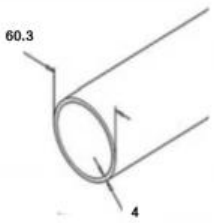
RON140-15
Weldable Base Plate
304/316



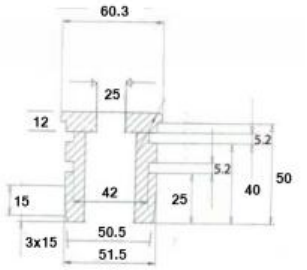
ROS140-61
Satin Cover Plate
304/316



ROS140-61-Mirror
Mirrored Cover Plate (316)

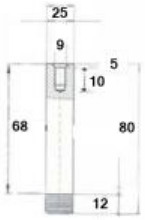


RO1001-60.3x4mm
(316G Satin 320Grit)



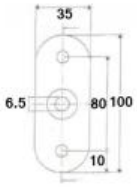
HH1060-60.3-316
Top Insert with 25mm threaded hole
316

HH1060-60.3-M8
Top Inser with M8 threaded hole
316

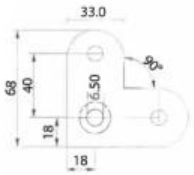


HH1002H-25-60.3
Fixed Stem - 316

GLS1002K-60.3-316
Stem with Swivel Neck



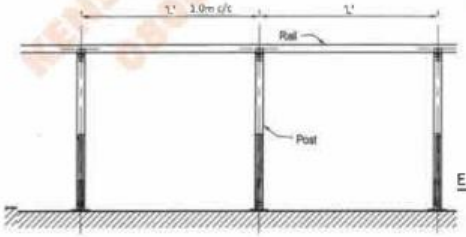
HH1001K-60.3-316
Straight Saddle



HH1001K-Z-60.3-316
90 Degree Corner Saddle

BALUSTRADING DESIGN

SECTION



ELEVATION

60.3CHS x 4 + 600mm high solid 50mm dia. Spiggot

HANDRAIL & POST DESIGN

MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 3.00Kn/m

γ_f = 1.60

HANDRAIL

$I_{xx} = \frac{\pi[60.3^4 - 52.5^4]}{64}$ = 276114.86mm^4

$Z_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{32 \times 60.3}$ = 9158.04mm^3

$S_{xx} = 0.167[60.3^3 - (60.3 - 2x3.9)^3]$ = 12450.37mm^3

ϵ = 1.22 Dlt = 15.46 = $(13.73\epsilon^3)$ section is Class1 - plastic

0.2% proof stress p_y = 220 N/mm^2

Factored lateral load applied to handrail = 3.0 x 1.6 = 4.80Kn/m

L = centres of posts

Applied M = $\frac{4.80 \times L^2}{8}$ = 0.60 L^2 Knm

Allowable M_c = $\frac{220 \times 12450.37}{10^6}$ = 2.74 Knm

or

$M_c = \frac{1.2 \times 220 \times 9158.04}{10^6}$ = 2.42 Knm

$0.60L^2 = 2.42$

$L = \sqrt{\frac{2.42}{0.60}}$ = 2.01m

Deflection

Limiting deflection to 25mm

$L = \sqrt[4]{\frac{25 \times 384 \times 200 \times 10^3 \times 276114.86}{5 \times 3.00 \times 10^9}}$ = 2.44m

MAXIMUM ALLOWABLE SPAN 2.0m

-2-

HANDRAIL & POST DESIGN

(60.3 x 4CHS post with 50mm dia solid Spiggot 600mm high)

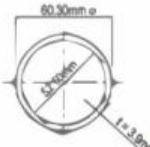
MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 3.00Kn/m

γ_f = 1.60

POST



$I_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{64}$ = 276114.86mm^4

$Z_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{32 \times 60.3}$ = 9158.04mm^3

$S_{xx} = 0.167[60.3^3 - (60.3 - 2x3.9)^3]$ = 12450.37mm^3

ϵ = 1.22 Dlt = 15.46 = $(10.39\epsilon^3)$ section is Class1 - plastic

0.2% proof stress p_y = 220 N/mm^2

Allowable M_c = $\frac{220 \times 12450.37}{10^6}$ = 2.74 Knm

or

$M_c = \frac{1.2 \times 220 \times 9158.04}{10^6}$ = 2.42 Knm

L = centres of posts

Applied moment 500mm below handrail

M = 4.8 x L x 0.5 = 2.40 L Knm

L = $\frac{2.42}{2.40}$ = 1.01m

deflection for post at 1.00m c/c

$\delta = \frac{3.0 \times 1.0 \times 10^3 \times 0.5^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 2.24mm satisfactory

HANDRAIL & POST DESIGN

(60.3 x 4 CHS post with 50mm dia solid Spiggot 600mm high)

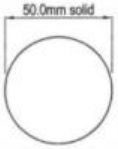
MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 3.00Kn/m

γ_f = 1.60

SPIGGOT



$I_{xx} = \frac{\pi 50^4}{64}$ = 306835.94mm^4

$Z_{xx} = \frac{\pi 50^3}{32}$ = 12273.44mm^3

say S_{xx} = 1.7 x 12273.44 = 20864.85mm^3

0.2% proof stress p_y = 220 N/mm^2

L = centres of posts

Allowable M_c = $\frac{220 \times 20864.85}{10^6}$ = 4.59 Knm

or

$M_c = \frac{1.2 \times 220 \times 12273.44}{10^6}$ = 3.24 Knm

at 500mm below handrail

load resisted by post - W_1 load resisted by spiggot - W_2

$W_1 - W_2 = \frac{(3.0 \times 1.0) 1.1}{0.6}$ = 5.50 Kn

and

$\frac{W_1}{276114.86} = \frac{W_2}{306835.94}$

W_1 = 2.61 Kn & W_2 = 2.89 Kn

Applied moment to post = 2.61 x 0.6 x 1.6 = 2.51 Knm

Applied moment to spiggot = 2.89 x 0.6 x 1.6 = 2.77 Knm

deflection for post at 1.00m c/c

$\delta = \frac{2.61 \times 10^3 \times 0.6^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 3.37mm satisfactory

relative deflection at top of post $\delta = \frac{1.42 \times 10^3 \times 1.1^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 11.29mm

PROVIDE 60.3CHS POST WITH 600mm SOLID 50mm dia. SPIGGOT AT 1.00m c/c

Do not risk your professional indemnity - use appropriate materials

POST BASEPLATE

MATERIAL - stainless steel grade 1.4401

Horizontal load 'H' applied at 1.10m above base plate level.

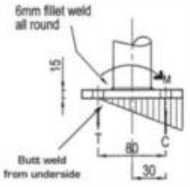
H= 3.0Kn/m (posts at 1.00m c/c)

γ_f = 1.60

M = 4.80 x 1.0 x 1.1 = 5.28 Knm

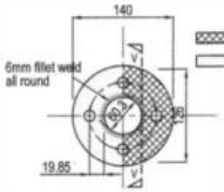
Lever Arm = 80mm

T = C = $\frac{5.28 \times 10^3}{80}$ = 66.00 Kn



i) Compression

Assuming rotation due to compression about V-V



$Z_{vv} = \frac{126 \times 15^2}{6}$ = 4725mm^3

0.2% proof stress p_y = 220 N/mm^2

$M_c = \frac{1.2 \times 220 \times 4725}{10^6}$ = 1.25 KNm

Moment in plate due to compression $M = \frac{66.00 \times 0.4(70 - 30.15)10^3}{10^6}$ = 1.05 KNm satisfactory

MAXIMUM ALLOWABLE POST CENTRES 1.00m

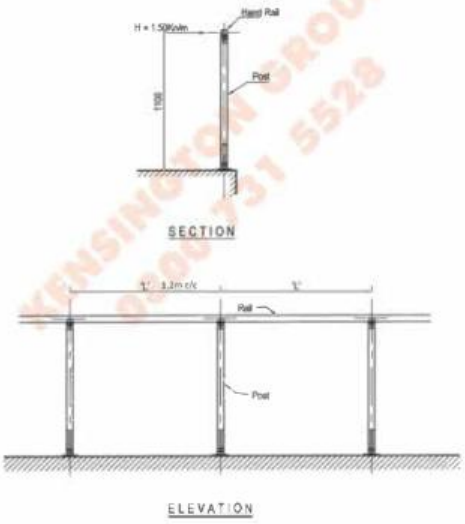
i) Tension

0.2 %proof stress p_y = 220 N/mm^2

Moment in plate due to bolt tension $M = \frac{66.00 (19.85 - \frac{6}{2}) 10^3}{10^6}$ = 0.91 KNm satisfactory

MAXIMUM ALLOWABLE POST CENTRES 1.00m

BALUSTRADING DESIGN



60.3CHS x 4 + 300mm high 50.8CHS x 3.0 Spiggot

HANDRAIL & POST DESIGN

MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 1.50Kn/m

γ_f = 1.60

HANDRAIL

60.30mm ø

52.50mm

t = 3.0mm

$I_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{64}$ = 276114.86mm^4

$Z_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{32 \times 60.3}$ = 9158.04mm^3

$S_{xx} = 0.167[60.3^3 - (60.3 - 2x3.9)^3]$ = 12450.37mm^3

ϵ = 1.22 D/t = 15.46 = (13.73ϵ^2) section is Class1 - plastic

0.2 % proof stress p_y = 220 N/mm^2

Factored lateral load applied to handrail = 1.5 x 1.6 = 2.40Kn/m

Applied M = $\frac{2.40 \times L^2}{8}$ = 0.30 L^2 Knm

Allowable M_c = $\frac{220 \times 12450.37}{10^6}$ = 2.74 Knm

or

M_c = $\frac{1.2 \times 220 \times 9158.04}{10^6}$ = 2.42 Knm

0.30 L^2 = 2.42

$\therefore L = \sqrt{\frac{2.42}{0.30}}$ = 2.84m

Deflection

Limiting deflection to 25mm

$L = \sqrt[4]{\frac{25 \times 384 \times 200 \times 10^3 \times 276114.86}{5 \times 1.50 \times 10^{12}}}$ = 2.90m

MAXIMUM ALLOWABLE SPAN 2.84m

HANDRAIL & POST DESIGN

(60.3 x 4 HS post with 50.8 x 3.0 Spiggot 300mm high) MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 1.50Kn/m

γ_f = 1.60

POST

60.30mm ø

52.50mm

t = 3.0mm

$I_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{64}$ = 276114.86mm^4

$Z_{xx} = \frac{\pi(60.3^4 - 52.5^4)}{32 \times 60.3}$ = 9158.04mm^3

$S_{xx} = 0.167[60.3^3 - (60.3 - 2x3.9)^3]$ = 12450.37mm^3

ϵ = 1.22 D/t = 15.46 = (10.39ϵ^2) section is Class1 - plastic

0.2 % proof stress p_y = 220 N/mm^2

Allowable M_c = $\frac{220 \times 12450.37}{10^6}$ = 2.74 Knm

or

M_c = $\frac{1.2 \times 220 \times 9158.04}{10^6}$ = 2.42 Knm

Applied moment 800mm below handrail

M = 2.4 x L x 0.8 = 1.92 L Knm

L = $\frac{2.42}{1.92}$ = 1.26m

deflection for post at 1.20m c/c

$\delta = \frac{1.5 \times 1.2 \times 10^3 \times 0.8^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 5.5mm satisfactory

HANDRAIL & POST DESIGN

(60.3 x 4 CHS post with 50.8 x 3.0 Spiggot 300mm high)

MATERIAL - stainless steel grade 1.4401 (316) [p_y = 220 N/mm^2]

Horizontal load 'H' applied at 1.10m above base plate level.

H= 1.50Kn/m

γ_f = 1.60

SPIGGOT

50.80mm ø

44.80mm

t = 3.0mm

L = centres of posts

$I_{xx} = \frac{\pi(50.8^4 - 44.8^4)}{64}$ = 129189.87mm^4

$Z_{xx} = \frac{\pi(50.8^4 - 44.8^4)}{32 \times 50.8}$ = 5086.22mm^3

$S_{xx} = 0.167[50.8^3 - 44.8^3]$ = 6877.25mm^3

ϵ = 1.22 D/t = 16.93 = (11.37ϵ^2) section is Class1 - plastic

0.2 % proof stress p_y = 220 N/mm^2

Allowable M_c = $\frac{220 \times 6887.25}{10^6}$ = 1.52 Knm

or

M_c = $\frac{1.2 \times 220 \times 5086.22}{10^6}$ = 1.34 Knm

at 800mm below handrail

load resisted by post - W_1 load resisted by spiggot - W_2

$W_1 + W_2 = \frac{(1.5 \times 1.2)1.1}{0.3}$ = 6.60 Kn

and

$\frac{W_1}{276114.86} = \frac{W_2}{129189.87}$

W_1 = 4.49 Kn & W_2 = 2.11 Kn

Applied moment to post = 4.49 x 0.3 x 1.6 = 2.16 Knm

Applied moment to spiggot = 2.11 x 0.3 x 1.6 = 1.01 Knm

deflection for post at 1.20m c/c

$\delta = \frac{4.49 \times 10^3 \times 0.3^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 0.72mm satisfactory

relative deflection at top of post $\delta = \frac{1.22 \times 10^3 \times 1.1^3 \times 10^9}{3 \times 200 \times 10^3 \times 279114.86}$ = 9.70mm

PROVIDE 60.3CHS POST WITH 300mm 50.8CHS x 3.0 SPIGGOT AT 1.20m c/c

POST BASEPLATE

MATERIAL - stainless steel grade 1.4401

Horizontal load 'H' applied at 1.10m above base plate level.

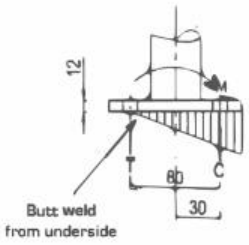
H= 1.50Kn/m (posts at 1.20m c/c)

γ_f = 1.60

M = 2.40 x 1.2 x 1.1 = 3.17 Knm

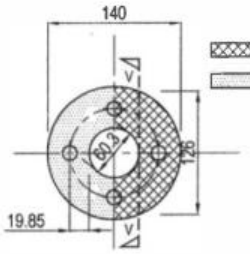
Lever Arm = 80mm

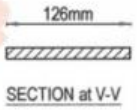
T = C = $\frac{3.17 \times 10^3}{80}$ = 39.63 Kn



i) Compression

Assuming rotation due to compression about V-V





$Z_{v-v} = \frac{126 \times 12^2}{6}$ = 3024mm^3

0.2 % proof stress p_y = 220 N/mm^2

$M_c = \frac{1.2 \times 220 \times 3024}{10^6}$ = 0.79 KNm

Moment in plate due to compression $M = \frac{39.63 \times 0.4(70 - 30.15)10^3}{10^6}$ = 0.63 KNm ∴ satisfactory

MAXIMUM ALLOWABLE POST CENTRES 1.20m

i) Tension

0.2 % proof stress p_y = 220 N/mm^2

Moment in plate due to bolt tension $M = \frac{39.63 \times 19.85 \times 10^3}{10^6}$ = 0.79 KNm ∴ satisfactory

MAXIMUM ALLOWABLE POST CENTRES 1.20m